

Modeling the J-Pole Antenna

A Deep Dive Presentation

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March 2024

Proposed:

- A J-Pole antenna will be modeled for computer simulation using the NEC antenna simulation engine developed by the Lawrence-Livermore Laboratory in the 1970s.
- We will be using the
 - EZNEC and
 - This application is particularly useful for presentations and beginners of antenna modeling.
 - 4NEC2 implementations of the NEC engine.
 - This application is more useful for the skilled NEC user owing to its symbology facilitation.
- Recommend that the viewer have reviewed the earlier [“qualitative” presentation](#).
 - [The basics of modeling the J-Pole for simulation](#).
- This will be a deep-dive into the actual modeling.
 - An Excel spreadsheet will be presented.
 - “Deep Dive” is not intended to mean “for rocket scientists only.”
 - Nothing beyond what is expected of amateur extra class licensees will be presented.

Questions You Must Consider

- What is a computer antenna model?
 - An architecture of wires with stimulus
- What knowledge do you need?
 - Success in modeling and simulation can only be of value if you already know most of the answers.
 - You understand what the pieces are doing
 - Might not understand their workings together
- Why Model Antennas?
 - Apply changes to what you already know to be true
- What are must-haves
 - Objectives
 - What answers are sought?

Why Model the J-Pole Antenna?

- The workings of the J-Pole are fully understood.
- Value-Add
 - Little operational value can be gained by simulating a J-Pole antenna.
- Ideal subject matter for learning NEC modeling
 - We know what the J-Pole is supposed to be doing
 - Does our model reflect that?
 - If yes---you are learning.
 - If no—what have you missed.

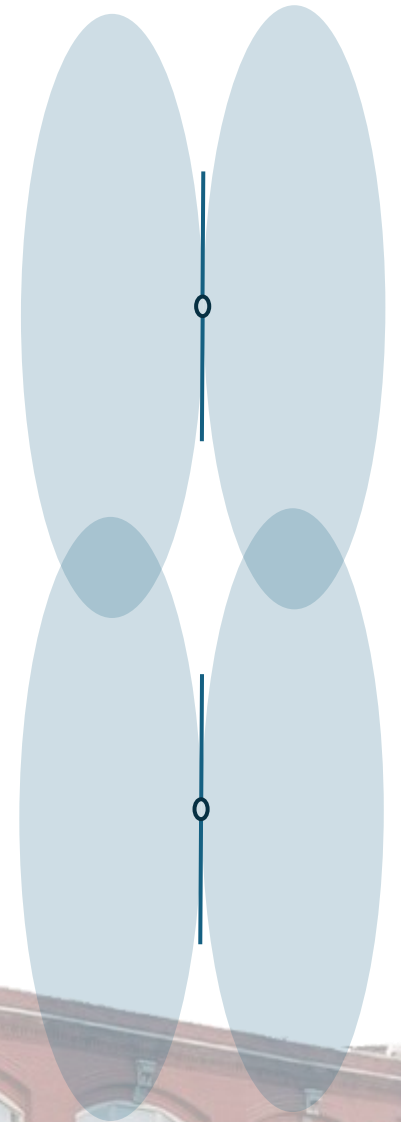
Benefits of Antenna Modeling



- Can serve as a second witness to a proof-of-concept for a design.
- Can model without parasitics to confirm anomalies.
- Useful in idea or concept value.
- Can provide information for otherwise unavailable information.

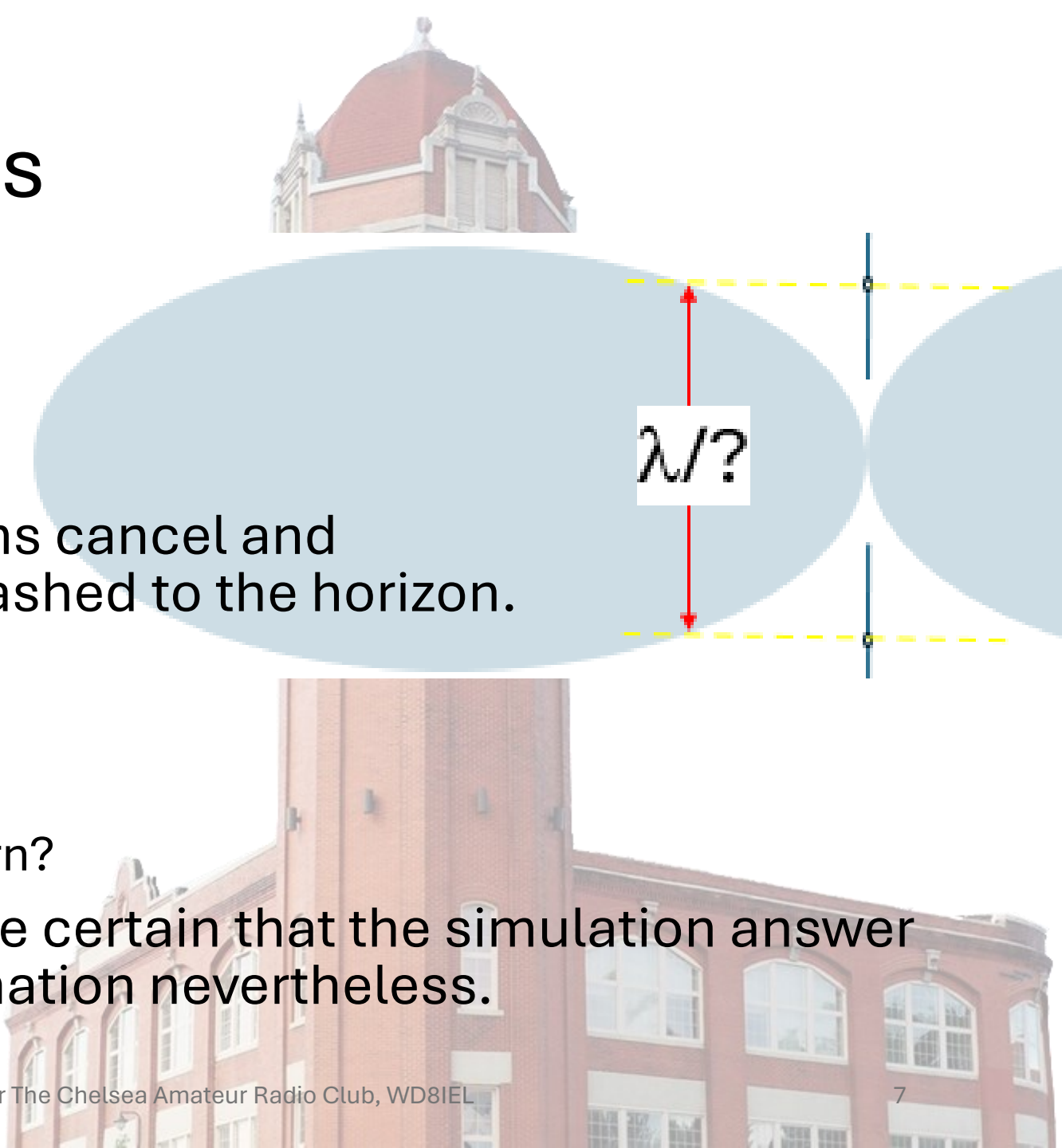
Example of Usefulness

- Devise a scheme whereby a pair of center-fed dipoles, stacked vertically, generate an omnidirectional flattened pattern.
- The doughnut pattern is to be squashed so as to send less energy to the moon and more to the horizon.
- What distance needs to exist between the centers of the antennas?



Example of Usefulness

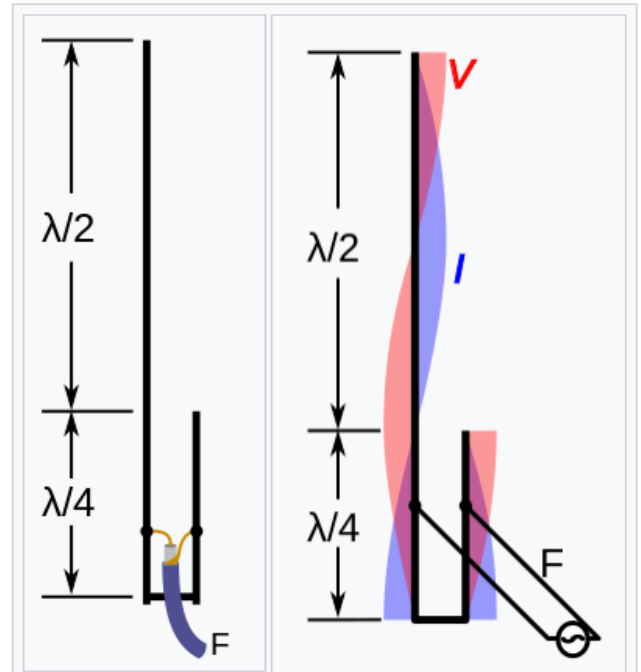
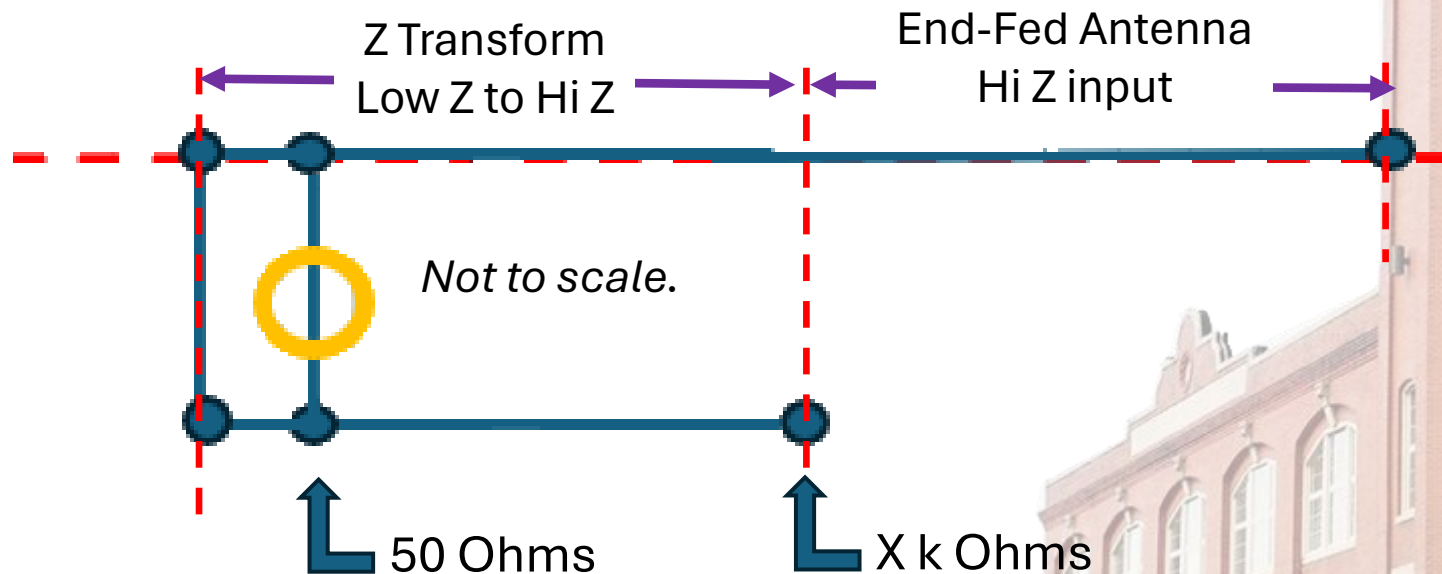
- There exists a
 - Phase difference and
 - Feed-point separation distance
- Such that the doughnut patterns cancel and add that the net pattern is squashed to the horizon.
- Questions
 - What phase difference and
 - What feed-point distance
 - Is required for a squashed pattern?
- Without a witness we cannot be certain that the simulation answer is correct but it is useful information nevertheless.



The J-Pole Components

J-pole antenna - Wikipedia

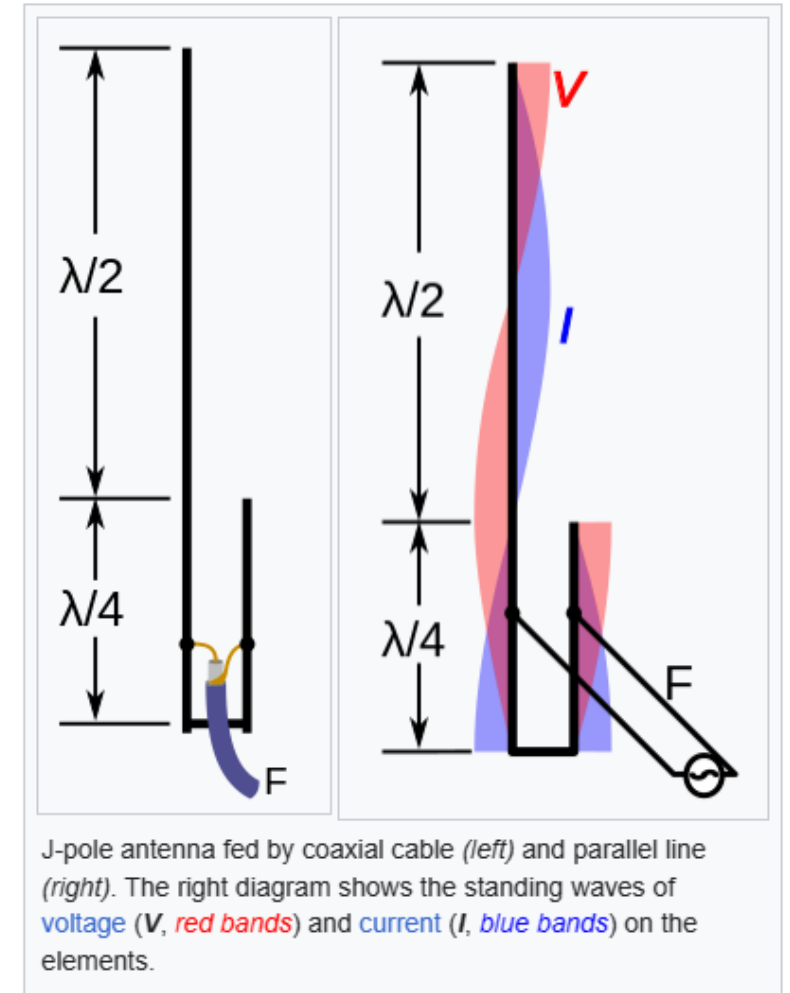
- The actual antenna
- A Z-transformer
 - Unfold revealing center-fed dipole
 - Z at the center is 50 Ohms
 - Z at the ends is several thousand—High Z



J-pole antenna fed by coaxial cable (left) and parallel line (right). The right diagram shows the standing waves of voltage (V, red bands) and current (I, blue bands) on the elements.

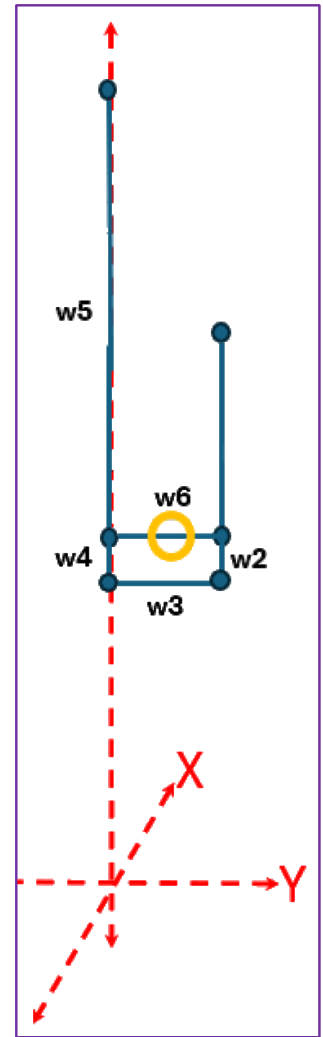
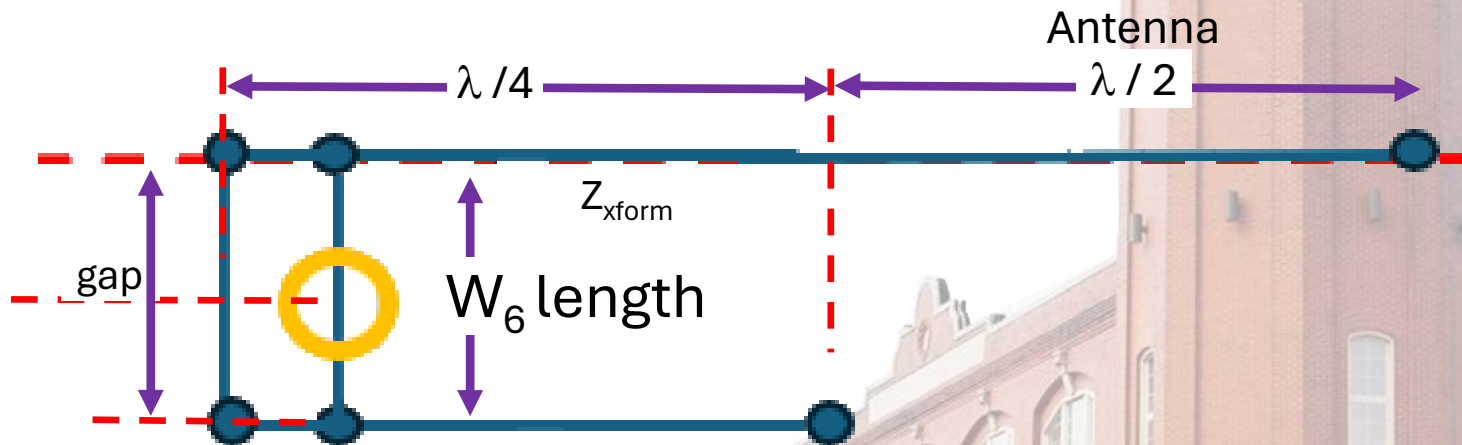
J-Pole Impedance Transformations

- The actual antenna is $\lambda/2$
 - Is end-fed
 - Therefore, is a high-Z input (typically 3 to 10 k Ω)
- Z_{xform}
 - low-Z input
 - High-Z output
- End-Fed antennas have a Hi-Z input Z.



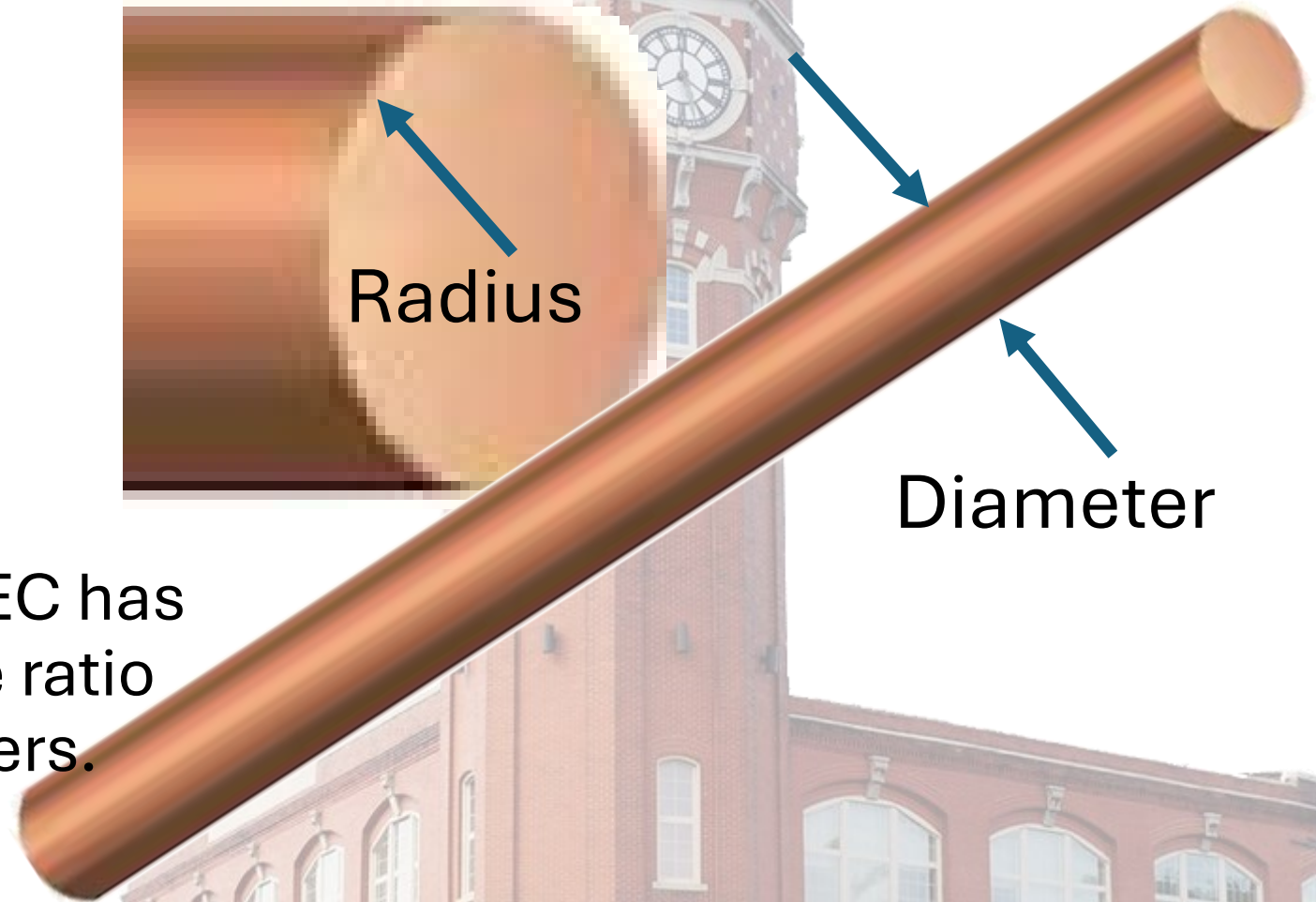
J-Pole Component Lengths

- The actual antenna is $\lambda/2$
- Z_{xform} length
 - Is $\lambda/4$
 - Unfold and xformer becomes a half-wave dipole, center fed.



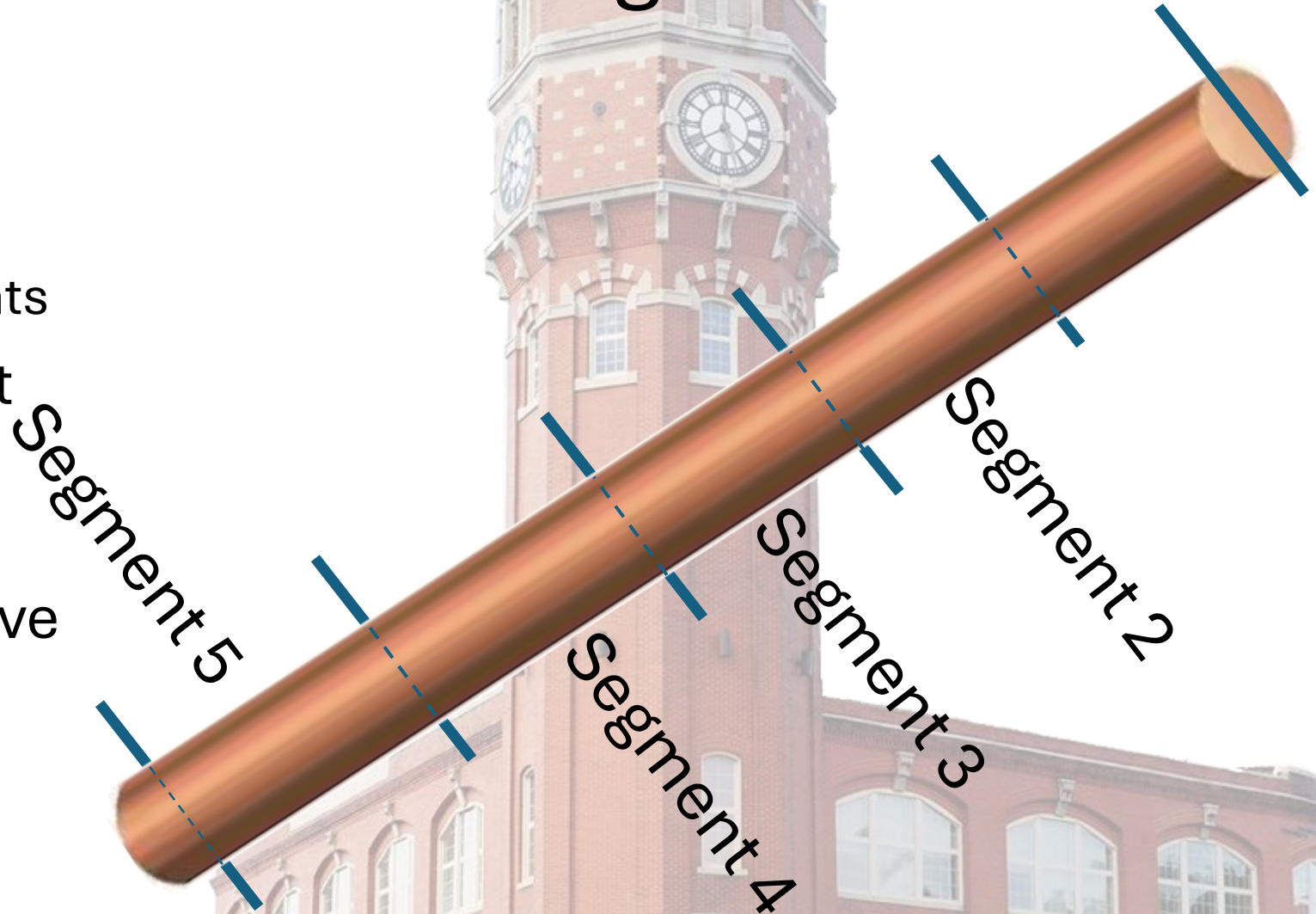
Antenna is Defined as a Set of Wires

- Wires define the antenna
- These have specifications
 - Diameter
 - Composition (molecular structure)
 - Length
- The numerical engine of NEC has requirements regarding the ratio of lengths and wire diameters.



Critical Concept: Wires Have Segments

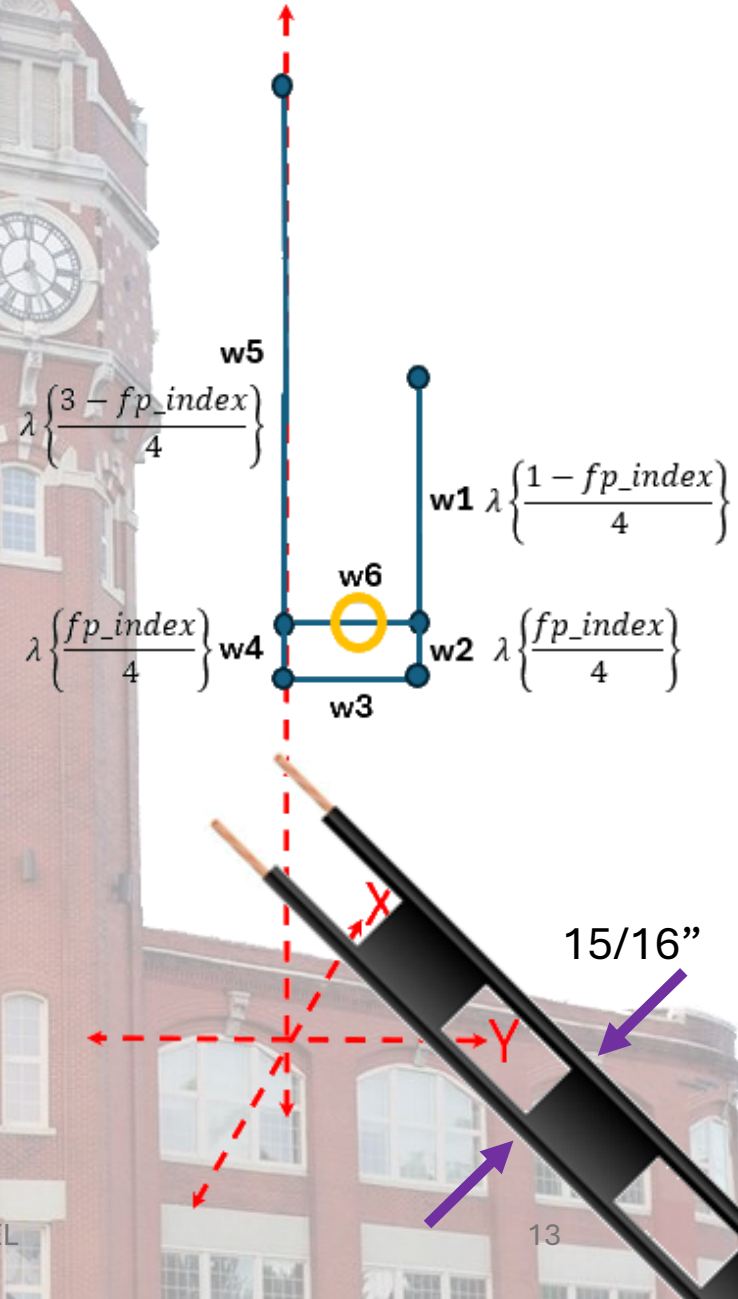
- An antenna wire
 - may have any length.
 - Is composed of segments
- The length of a segment
 - Has a minimum
 - Has a maximum
- A very long wire may have many segments.
- Each segment has a min/max limitation.



Define the Antenna Specifications

- Resonant frequency: 146 MHz
- Velocity factor: 1.0
 Note: For purposes of the NEC modeling software, we will ignore velocity factor. But that is only for now and for simplification purposes because of the nature of the NEC software.
- J-Pole Composition: Ladder Line
- Use AWG #12 Wire
 - Diameter = 0.002052 meters
- Wire lengths shown at right →
- Will solve for the segments per wire in slides.

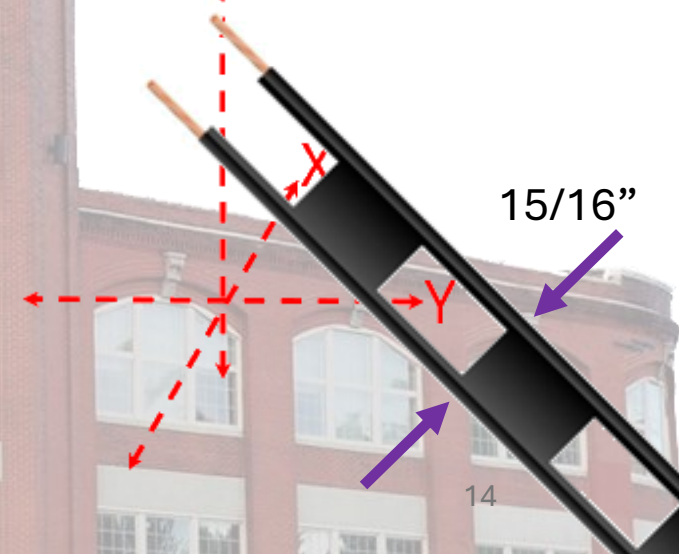
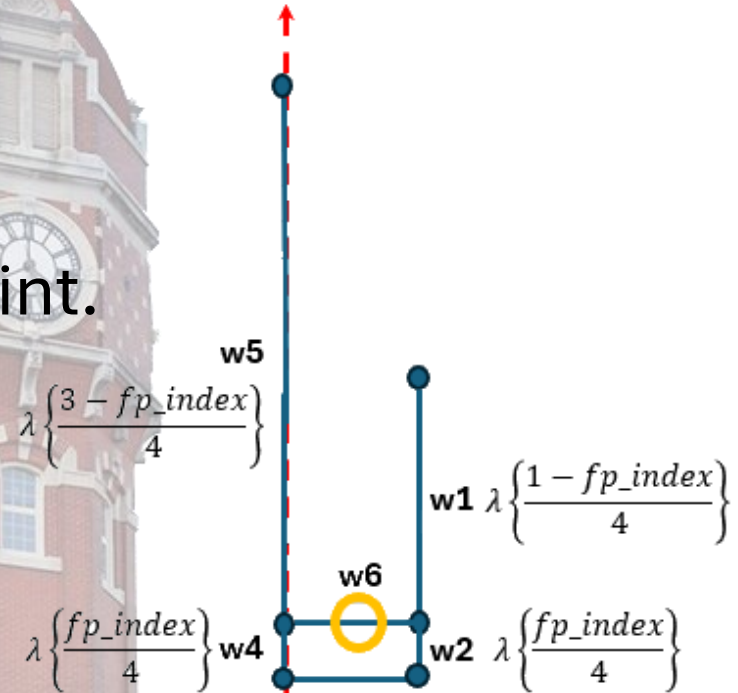
w#	End-to-End Needed (m)
w1	0.475769838
w2	0.025667163
w3	0.0238125
w4	0.025667163
w5	1.514362588
w6	0.0238125



Purpose of *fp_index* Variable

- A crap-shoot knowing where to place the feed point.
- The feed point defined here as a function of *fp_index*.
- Is the equivalent of sliding the feed point up and down trombone style.
- Facilitates ease of iteration for a solution.

w#	End-to-End Needed (m)
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w6	0.0238125



Rule #1: Wire Segment Maximum Length

- The official rule: NEC requires: *Segment Lengths* $< \lambda/10$
- EZNEC requires *Segment Lengths* $< \lambda/18$
- All things considered, lets use *Segment Lengths* $< \lambda/20$
 - For convenience: ***SegLen*** $< \frac{c}{20 \text{ freq}}$
 - $\lambda / 20 = 2.053356 \text{ m} / 20 = 0.1026678 \text{ m}$
 - This applies to all wire segment lengths used anywhere in this design.

Test W_5 for a Maximum Length

- W_5 length is 1.5144 meters
- Truth test:
 - is $1.51 \text{ m} < 0.1026 \text{ m} \rightarrow \text{FALSE}$
- What must be done
 - W_5 must have **AT LEAST** $1.51/0.1026 = 14.7$ segments
 - Segments only come in integer values
 - **W_5 must have at least 15 segments**

w#	End-to-End Needed (m)
w1	0.475769838
w2	0.025667163
w3	0.0238125
w4	0.025667163
w5	1.514362588
w6	0.0238125

Rule #2 a and b: Wire Segment Min Lengths

- NEC has two MINIMUM segment length requirements:

- $\lambda/1,000$
- 4 Wire Diameter

$< \text{Segment Length}$

- λ remains 2.053356 meters
- Min len #1: $\lambda/1,000 = 0.002053$ meters
- Min len #2: $4 * \text{Dia of \#12 wire} = 0.008100$ meters
- Segment lengths $>$ the greater of the two.

Wire Segment Minimum Lengths

$$\lambda/1,000 = 0.002053m$$

$$4 \text{ Wire Dia} = 0.0081m$$

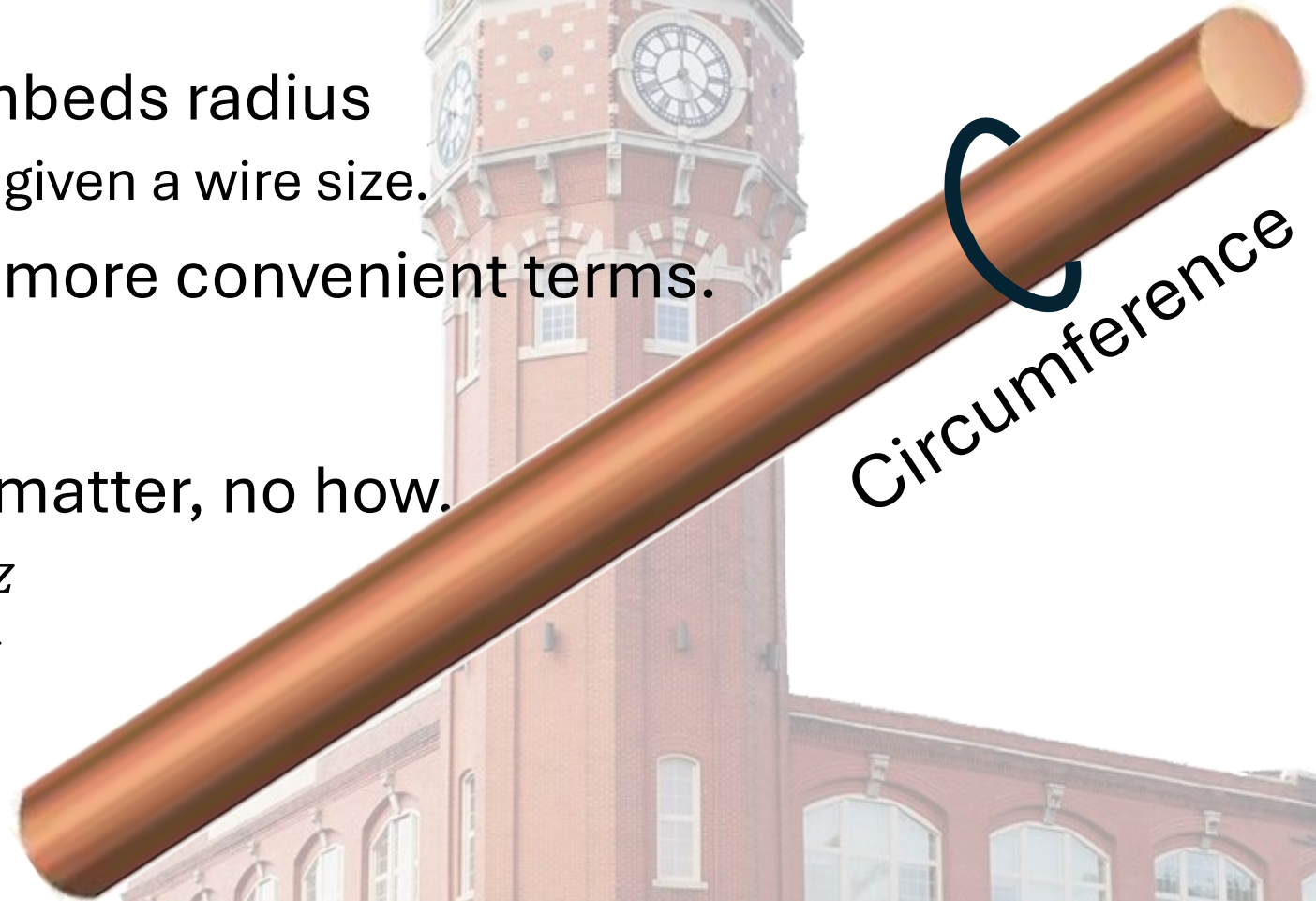
$$< 0.0081 \text{ Segment Length}$$

- What is the largest number of segments allowed for wire W_5 ?
- $1.514m/0.0081m = 186$
- Resulting requirement for W_5 :
 - $15 \leq W_5 \text{ \# Segments} \leq 186$

w#	End-to-End Needed (m)
w1	0.475769838
w2	0.025667163
w3	0.0238125
w4	0.025667163
w5	1.514362588
w6	0.0238125

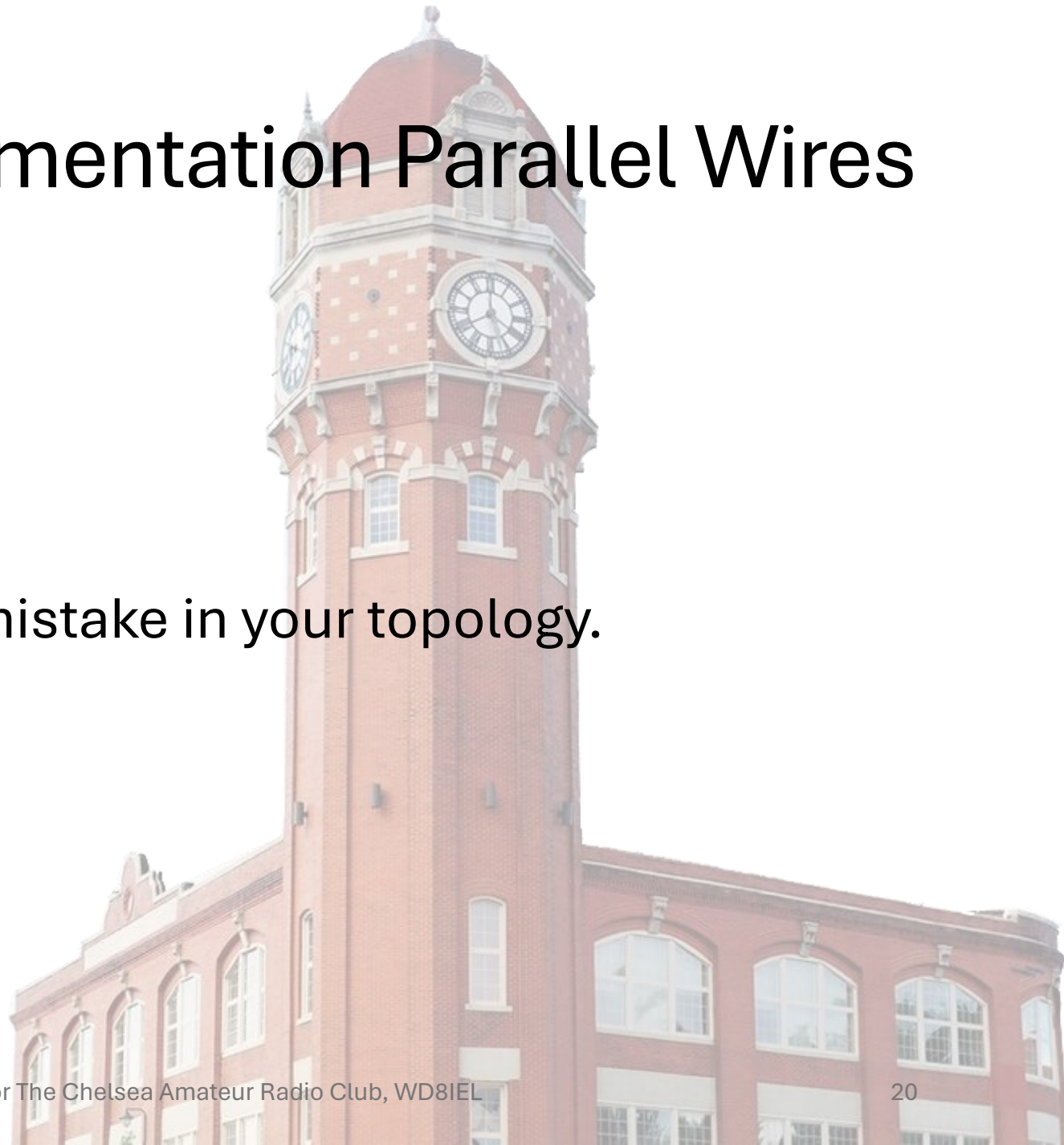
Rule #3: Circ $\rightarrow \frac{\text{circumference}}{\lambda} \ll \text{Unity}$

- Because circumference embeds radius
 - Max f_0 NEC may be used for given a wire size.
- This can be re-defined into more convenient terms.
 - $f_{o\ max}(GHz) \ll \frac{3e8m}{s}vf / \pi\ Diam$
- But how much less? Don't matter, no how.
 - #1 AWG wire: $f_0 < 0.82\ GHz$
 - #30 AWG wire: $f_0 < 75\ GHz$



Rule #4: Unequal Segmentation Parallel Wires

- Unequal Segmentation for
 - Parallel wires
 - Within $\lambda/20$ of each other
 - Having an overlap of $\lambda/10$.
- If you get this error, look for a mistake in your topology.



Relational Segment Lengths

- A segment length must not differ by more than 5x the segment length of another wire.



Special Case: Angled Joining of Wires

- Must not allow the center of one wire to enter the radius of another wire—these are corners.
 - Satisfied with: $\frac{\textit{Segment Length}}{\textit{Wire Diameter}} > 4$
- Re-written for convenience:
 - $\frac{\textit{Segment Length}}{4 \textit{ Wire Diameter}} > \textit{unity}$
- For w1
 - Will be using 5 segments
 - $0.4873\text{m} / (4 * 0.002052\text{m}) / 5\text{seg} = 11.8 > \textit{unity} \rightarrow \text{GOOD}$

Test Wire Maximum Segment Lengths

- Because all the wires are the same size
 - Max #1: $\lambda/20 = 0.10267$ m
 - Max #2: $4 * \text{dia}$
 - #12 AWG → Dia = 0.002052 m
 - $4 * \text{Dia} = 0.008208\text{m}$
 - Net Max is the lesser of the two
 - Max Seg Len = 0.008208 m
- Applicability
 - Because λ has one value
 - and there is one wire size
 - Max Seg Len = 0.008208 m

w#	End-to-End Needed (m)
w1	0.475769838
w2	0.025667163
w3	0.0238125
w4	0.025667163
w5	1.514362588
w6	0.0238125

Solve for Maximum Number of Segments

- MIN Segment length = 0.008208 m
- The MAXIMUM number of segments per wire may now be solved for.
 - $W_1 = 0.475/0.0082 = \text{FLOOR}(57.9) = 57$
 - $W_2 = W_4 = 0.02567/0.0082 = \text{FLOOR}(3.1) = 3$
 - $W_3 = W_6 = 0.0238125/0.0082 = \text{FLOOR}(2.9) = 2$
 - $W_5 = 1.514/0.0082 = \text{FLOOR}(184.6) = 184$

w#	End-to-End Needed (m)	Max
w1	0.475769838	57
w2	0.025667163	3
w3	0.0238125	2
w4	0.025667163	3
w5	1.514362588	184
w6	0.0238125	2

Solve for Minimum Number of Segments

- Max Segment length = 0.10266865 m
- The MINIMUM number of segments per wire may now be solved for.

- $W_1 = 0.475/0.103 = \text{CEILING}(4.6) = 5$
- $W_2 = W_4 = 0.02567/0.103 = \text{CEILING}(0.249) = 3$
- $W_3 = W_6 = 0.0238125/0.103 = \text{CEILING}(0.23) = 1$
- $W_5 = 1.514/0.103 = \text{CEILING}(14.7) = 15$

	Min	w#	End-to-End Needed (m)	Max
	5	w1	0.475769838	57
	1	w2	0.025667163	3
	1	w3	0.0238125	2
	1	w4	0.025667163	3
	15	w5	1.514362588	184
	1	w6	0.0238125	2

Arbitrarily Pick Number of Seg Per Wire

- It is an arbitrary decision at this point how many segments to specify per wire.
- Any values within those limits are acceptable.

Number Used	Min	w#	End-to-End Needed (m)	Max
11	5	w1	0.475769838	57
2	1	w2	0.025667163	3
1	1	w3	0.0238125	2
1	1	w4	0.025667163	3
22	15	w5	1.514362588	184
1	1	w6	0.0238125	2

EZNEC Offers Auto Segment



- A very handy feature to have available.

Wires

Wire Create Edit Other

Add...
Delete...
Move Wire(s) in List...
Group Modify...
Auto Seg >
Change Height by...
Change Loop Size...
Copy Wires...
Move Wires XYZ...
Rotate Wires...
Scale Wires...

Sections Show Wire Insulation Show Loss

Wires				
		End 2		
	Conn	X (m)	Y (m)	Z (m)
W3E1	0	0	0.023813	2.51334
W3E2	0	0	0.023813	2.02567
W3E3	0	0	0.023813	2.02567
W3E4	0	0	0.023813	2.02567
W3E5	0	0	0.023813	2.02567
W3E6	0	0	0.023813	2.02567
W3E7	0	0	0.023813	2.02567
W3E8	0	0	0.023813	2.02567
W3E9	0	0	0.023813	2.02567
W3E10	0	0	0.023813	2.02567
W3E11	0	0	0.023813	2.02567
W3E12	0	0	0.023813	2.02567
W3E13	0	0	0.023813	2.02567
W3E14	0	0	0.023813	2.02567
W3E15	0	0	0.023813	2.02567
W3E16	0	0	0.023813	2.02567
W3E17	0	0	0.023813	2.02567
W3E18	0	0	0.023813	2.02567
W3E19	0	0	0.023813	2.02567
W3E20	0	0	0.023813	2.02567
W3E21	0	0	0.023813	2.02567
W3E22	0	0	0.023813	2.02567
W3E23	0	0	0.023813	2.02567
W3E24	0	0	0.023813	2.02567
W3E25	0	0	0.023813	2.02567
W3E26	0	0	0.023813	2.02567
W3E27	0	0	0.023813	2.02567
W3E28	0	0	0.023813	2.02567
W3E29	0	0	0.023813	2.02567
W3E30	0	0	0.023813	2.02567
W3E31	0	0	0.023813	2.02567
W3E32	0	0	0.023813	2.02567
W3E33	0	0	0.023813	2.02567
W3E34	0	0	0.023813	2.02567
W3E35	0	0	0.023813	2.02567
W3E36	0	0	0.023813	2.02567
W3E37	0	0	0.023813	2.02567
W3E38	0	0	0.023813	2.02567
W3E39	0	0	0.023813	2.02567
W3E40	0	0	0.023813	2.02567
W3E41	0	0	0.023813	2.02567
W3E42	0	0	0.023813	2.02567
W3E43	0	0	0.023813	2.02567
W3E44	0	0	0.023813	2.02567
W3E45	0	0	0.023813	2.02567
W3E46	0	0	0.023813	2.02567
W3E47	0	0	0.023813	2.02567
W3E48	0	0	0.023813	2.02567
W3E49	0	0	0.023813	2.02567
W3E50	0	0	0.023813	2.02567
W3E51	0	0	0.023813	2.02567
W3E52	0	0	0.023813	2.02567
W3E53	0	0	0.023813	2.02567
W3E54	0	0	0.023813	2.02567
W3E55	0	0	0.023813	2.02567
W3E56	0	0	0.023813	2.02567
W3E57	0	0	0.023813	2.02567
W3E58	0	0	0.023813	2.02567
W3E59	0	0	0.023813	2.02567
W3E60	0	0	0.023813	2.02567
W3E61	0	0	0.023813	2.02567
W3E62	0	0	0.023813	2.02567
W3E63	0	0	0.023813	2.02567
W3E64	0	0	0.023813	2.02567
W3E65	0	0	0.023813	2.02567
W3E66	0	0	0.023813	2.02567
W3E67	0	0	0.023813	2.02567
W3E68	0	0	0.023813	2.02567
W3E69	0	0	0.023813	2.02567
W3E70	0	0	0.023813	2.02567
W3E71	0	0	0.023813	2.02567
W3E72	0	0	0.023813	2.02567
W3E73	0	0	0.023813	2.02567
W3E74	0	0	0.023813	2.02567
W3E75	0	0	0.023813	2.02567
W3E76	0	0	0.023813	2.02567
W3E77	0	0	0.023813	2.02567
W3E78	0	0	0.023813	2.02567
W3E79	0	0	0.023813	2.02567
W3E80	0	0	0.023813	2.02567
W3E81	0	0	0.023813	2.02567
W3E82	0	0	0.023813	2.02567
W3E83	0	0	0.023813	2.02567
W3E84	0	0	0.023813	2.02567
W3E85	0	0	0.023813	2.02567
W3E86	0	0	0.023813	2.02567
W3E87	0	0	0.023813	2.02567
W3E88	0	0	0.023813	2.02567
W3E89	0	0	0.023813	2.02567
W3E90	0	0	0.023813	2.02567
W3E91	0	0	0.023813	2.02567
W3E92	0	0	0.023813	2.02567
W3E93	0	0	0.023813	2.02567
W3E94	0	0	0.023813	2.02567
W3E95	0	0	0.023813	2.02567
W3E96	0	0	0.023813	2.02567
W3E97	0	0	0.023813	2.02567
W3E98	0	0	0.023813	2.02567
W3E99	0	0	0.023813	2.02567
W3E100	0	0	0.023813	2.02567

Conservative
Minimum Recommended

> **6-Meter 3 element wide-b**

File JPole Classic Model.EZ

NEC Wire Table

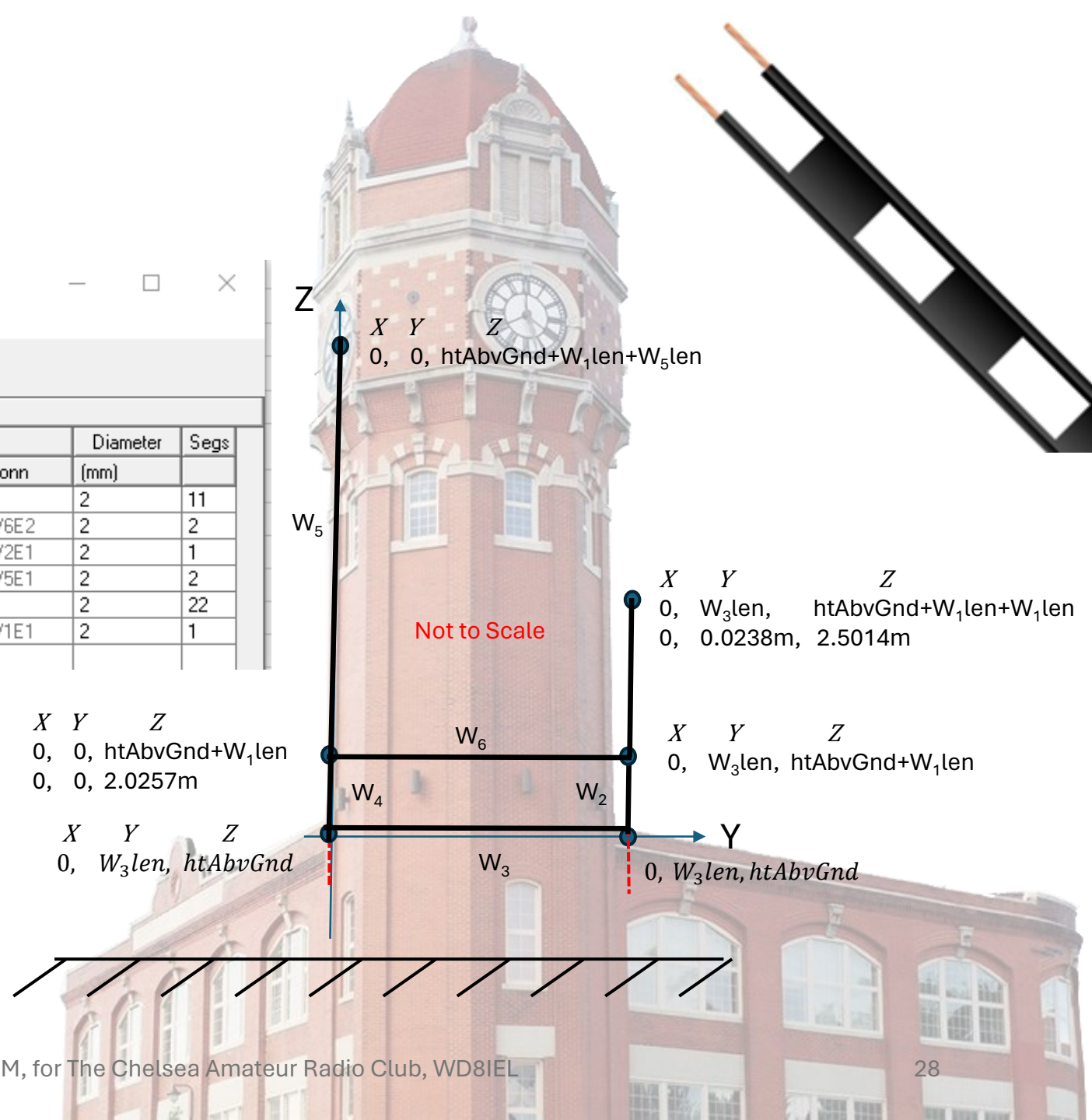
Wires

Wire Create Edit Other

Coord Entry Mode Preserve Connections Show Wire Insulation

Wires											
No.	End 1				End 2				Diameter (mm)	Segs	
	X (m)	Y (m)	Z (m)	Conn	X (m)	Y (m)	Z (m)	Conn			
1	0	0.023813	2.02567	W2E2	0	0.023813	2.50144		2	11	
2	0	0.023813	2	W3E2	0	0.023813	2.02567	W6E2	2	2	
3	0	0	2	W4E1	0	0.023813	2	W2E1	2	1	
4	0	0	2	W3E1	0	0	2.02567	W5E1	2	2	
5	0	0	2.02567	W6E1	0	0	3.52812		2	22	
6	0	0	2.02567	W4E2	0	0.023813	2.02567	W1E1	2	1	

- A table defines the topology of the antenna.

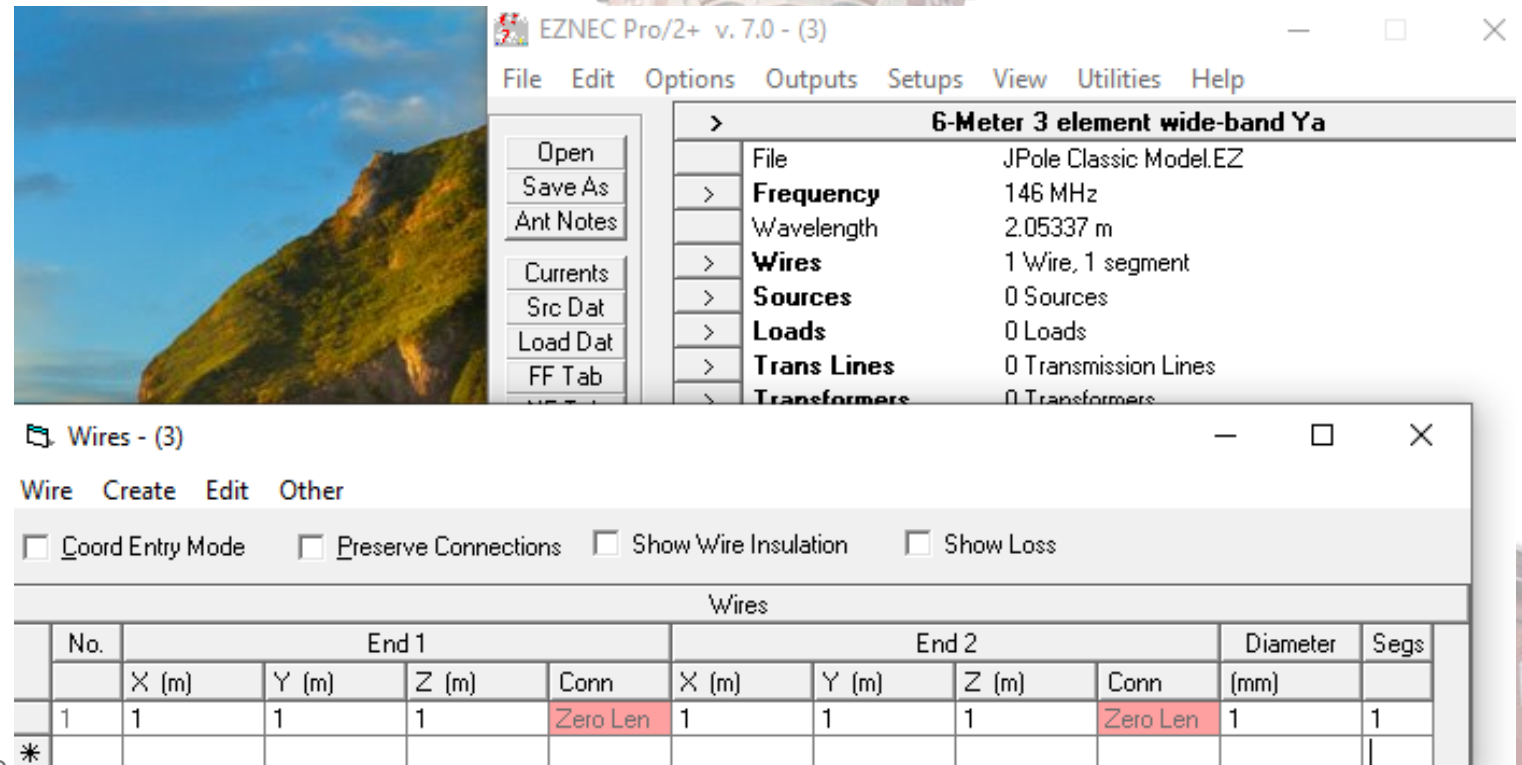


Wes' Excel Spreadsheet



Steps to Input to EZNEC

- Define the resonant frequency of the antenna.
- Define the ground options
- Define the wire list



The screenshot displays the EZNEC Pro/2+ v. 7.0 software interface. The main window shows the project settings for a "6-Meter 3 element wide-band Ya" antenna. The settings include:

- File: JPole Classic Model.EZ
- Frequency: 146 MHz
- Wavelength: 2.05337 m
- Wires: 1 Wire, 1 segment
- Sources: 0 Sources
- Loads: 0 Loads
- Trans Lines: 0 Transmission Lines
- Transformers: 0 Transformers

The "Wires" window is open, showing a table with the following data:

No.	End 1				End 2				Diameter (mm)	Segs
	X (m)	Y (m)	Z (m)	Conn	X (m)	Y (m)	Z (m)	Conn		
1	1	1	1	Zero Len	1	1	1	Zero Len	1	1

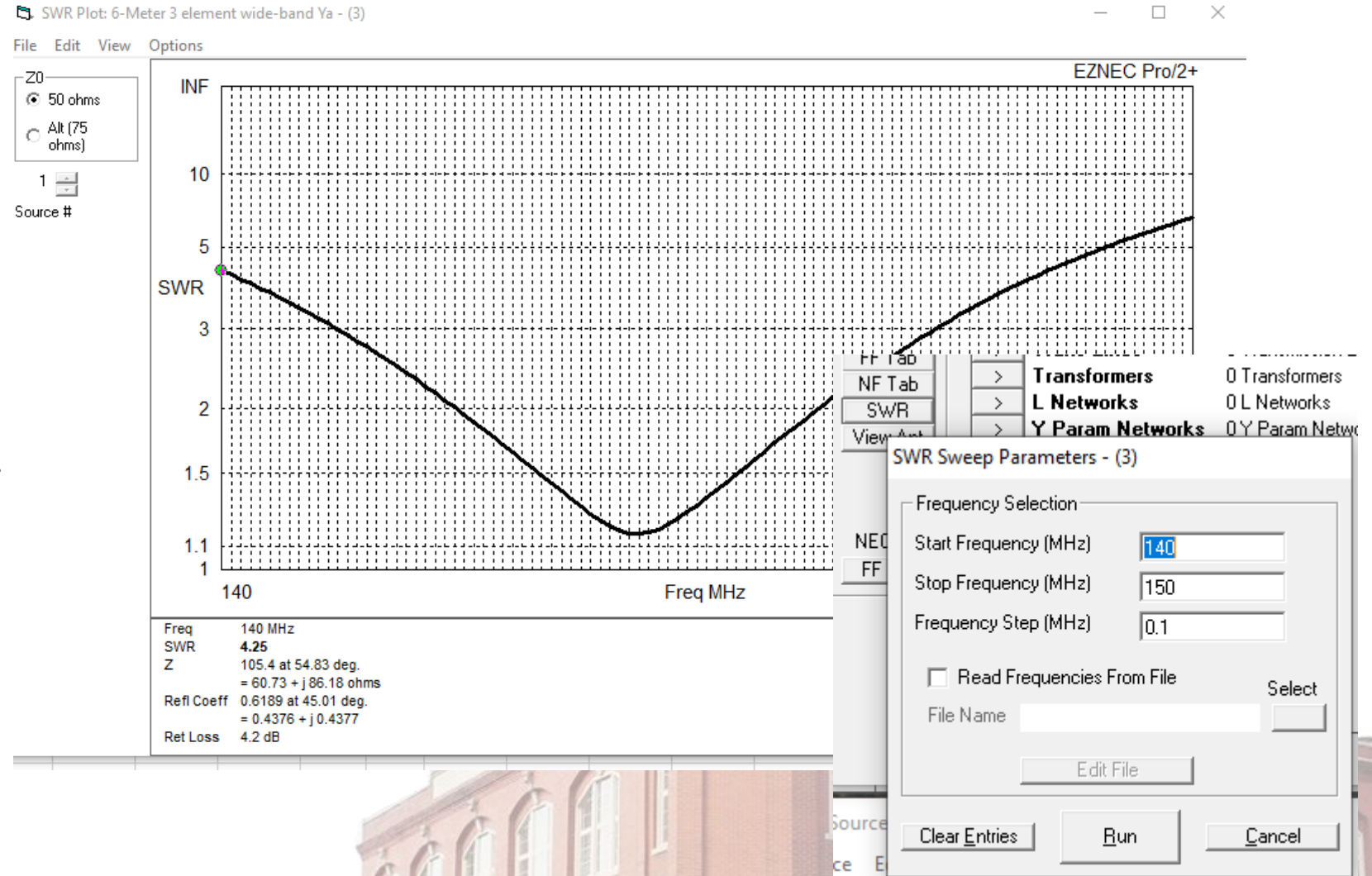
Defining the Wire List

- Type in the wire list
- The format is:

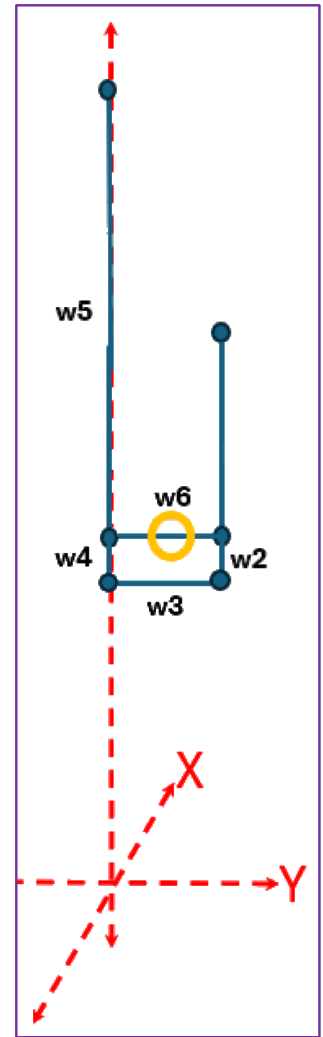
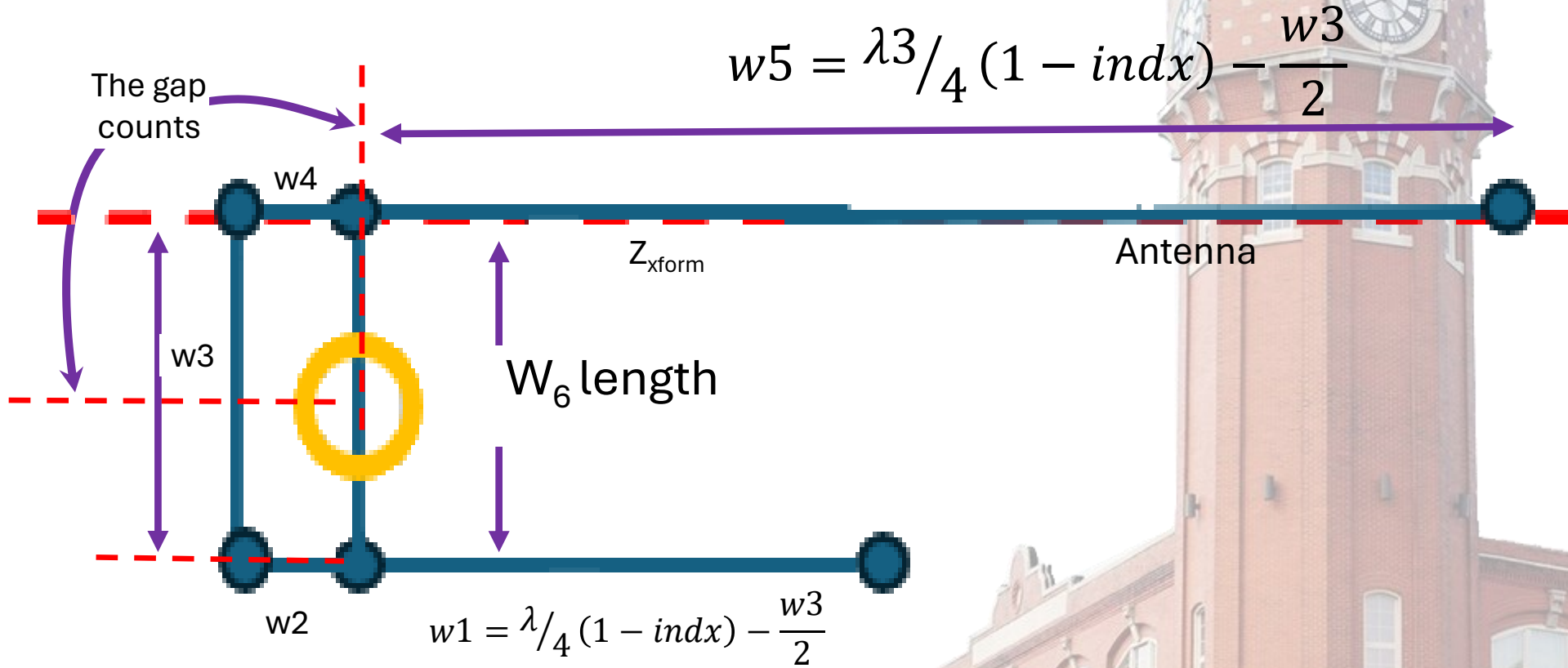
End 1				End2				Dia(mm)	# Segments
X	Y	Z	Conn	X	Y	Z	Conn		
0	0.023813	2.02567		0	0.023813	2.051334		2.05232	11
0	0.023813	2		0	0.023813	2.025667		2.05232	2
0	0	2		0	0.023813	2		2.05232	2
0	0	2		0	0	2.025667		2.05232	2
0	0	2.02567		0	0	3.54003		2.05232	22
0	0	2.02567		0	0.023813	2.025667		2.05232	1

Plot the SWR

- Not very impressive.
- Resonates at 144 MHz
- Consider the gap.



Wes' Stuff Closer Up



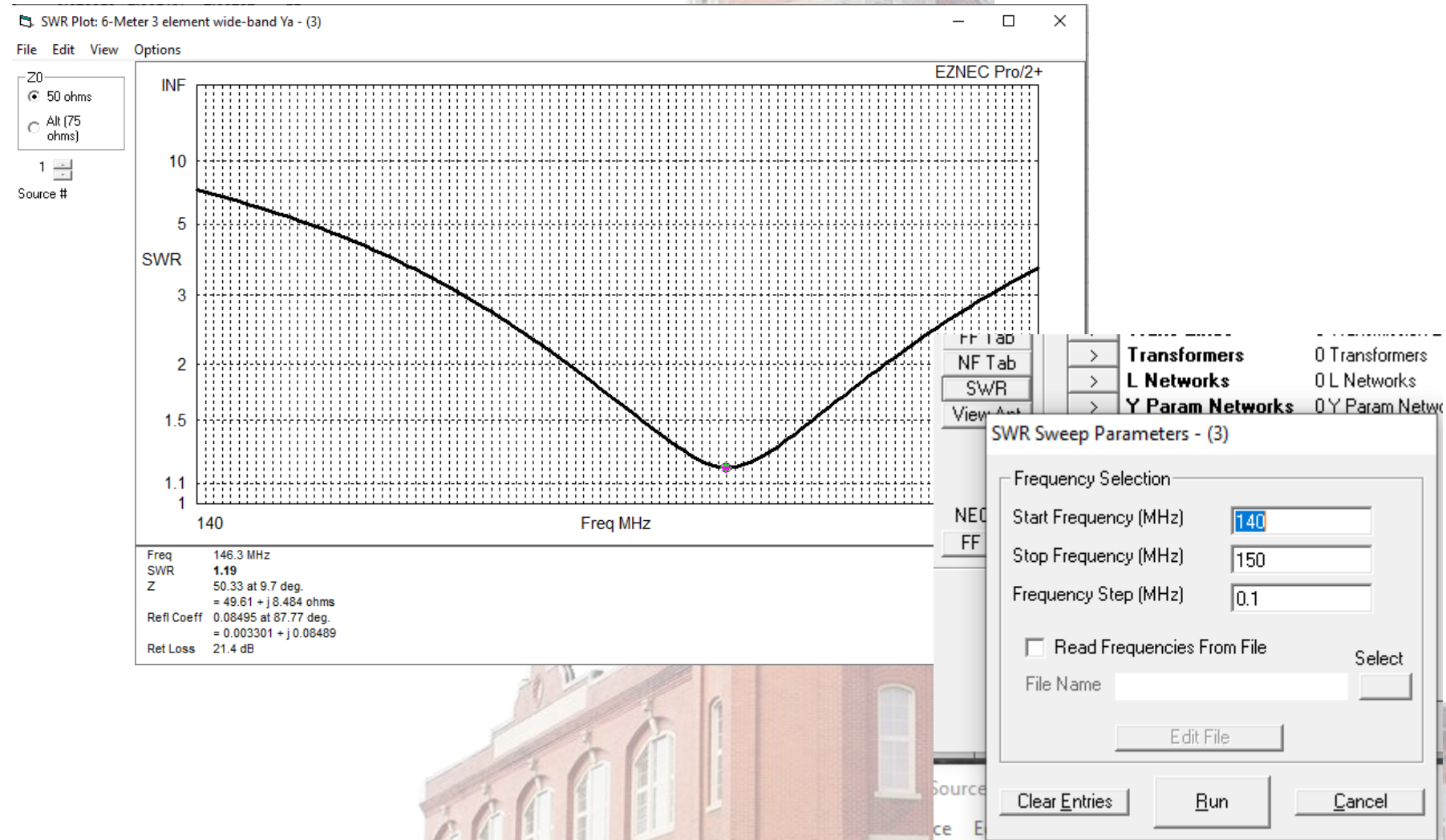
Defining the Wire List

- Make two changes to account for the “missing” gap

	End 1				End2					
•	X	Y	Z	Conn	X	Y	Z	Conn	Dia(mm)	# Segments
•	0	0.023813	2.02567		0	0.023813	3 2.0501437		2.05232	11
•	0	0.023813	2		0	0.023813	2.025667		2.05232	2
•	0	0	2		0	0.023813	2		2.05232	2
•	0	0	2		0	0	2.025667		2.05232	2
•	0	0	2.02567		0	0	3.528124		2.05232	22
•	0	0	2.02567		0	0.023813	2.025667		2.05232	1

Plot the Revised SWR

- impressive.
- Resonates at 146.3 MHz



What About our Feed Point Entry Point?

- We guessed at a value of 0.05
- It was a good guess but can still be optimized.
- I've tried
 - 0.04 which returns an SWR of 1.5.
 - 0.07 which was but resonating at 148 MHz.
- But don't forget that we have been using a velocity factor of unity.